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(54) **Mosfet AC switch.**

(57) A solid state relay is responsive to a control signal and is used with an impedance load and a source of alternating electrical power. The solid state relay is used to connect and disconnect the load from the source of alternating electrical power. The solid state relay turns on in response to a control signal and to a substantially zero voltage crossing of the alternating electrical power of the source. The solid state relay turns off in response to the control signal and to a substantially zero current crossing of the alternating electrical power of the source.

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Background of the Invention

The present invention relates in general to solid state relays and, in particular, to solid state relays and AC switches using MOSFET devices.

05 Compared to electromechanical relays, solid state relays have several advantages. These advantages include a longer lifetime, the elimination of contact bounce, and low voltage turn on that reduces both the
10 electromagnetic interference and stress on the attached load. Typical prior art solid state relays utilize triac and SCR components for the switching device. These components when used in a solid state relay have a number of disadvantages. These solid state relays
15 usually are very costly to manufacture, have high leakage current, and are prone to false triggering. Also prior art solid state relays are not readily compatible for use with high impedance logic circuits and CMOS logic.

The present invention overcomes the drawbacks in
20 the prior art solid state relays by the novel use of MOSFET devices.

Summary of the Invention

The present invention involves a solid state relay responding to a control signal and for use with an
25 impedance load and a source of alternating electrical power. The control signal is used to indicate when the solid state relay is to connect the impedance load to the source. The solid state relay uses two MOSFET devices wired in series in a source to source
30 configuration. The load is connected in series with the MOSFET devices and the total series circuit is

connected across the AC source. A portion of the circuitry in the solid state relay operates to turn on the solid state relay in response to the control signal and to a zero voltage crossing of the alternating electrical power of the source. Another portion of the circuitry of the solid state relay provides for turning off the solid state relay responsive to the control signal and to a zero current crossing of the alternating electrical current flowing through the load.

Objects of the Invention

It is a primary object of the present invention to provide a novel solid state relay especially for low power AC applications. It is another object of the present invention to provide a solid state relay which prevents false triggering and minimizes switch dissipation.

It is yet another object of the present invention to provide a solid state relay which is readily compatible with high impedance logic circuits and CMOS logic.

It is another object of the present invention to provide a solid state relay which turns on only at a zero voltage crossing point of the alternating source voltage.

It is a further object of the present invention to provide a solid state relay which turns off only at a zero current crossing point of the alternating source current.

Brief Description of the Drawings

The features of the present invention which are believed to be novel are set forth with particularity in the appended claims. The invention
05 together with further objects and advantages may best be understood by reference to the following description taken in conjunction with the accompanying drawings, in the several figures of which like reference numerals identify like elements, and in which:

10 Figure 1 is a general block diagram of the solid state relay.

Figure 2 is a graph comparing the timing of various signals in the solid state relay.

Figure 3 is a more specific block diagram
15 with circuit elements of the Figure 1 diagram.

Figure 4A and 4B are graphs of signals in the Figure 3 circuit.

Description of Preferred Embodiment

The novel solid state relay of the present
20 invention is shown in general block diagram form in Figure 1. An alternating power source 10 is connected between a hot node A and a neutral node N. An impedance load 12 is connected between node B and node N. A first switch 14 is connected in series with a
25 second switch 16 at common node C and the combination is connected between nodes A and B and in series with the load 12. Thus, when the first and second switches 14 and 16 are closed the load 12 is connected across the alternating power source 10. A floating power
30 supply 18 is referenced to node C and provides a voltage to power the control circuit 20. The control

circuit 20 controls the first and second switches 14 and 16 on output line 22. The control circuit 20 receives a control signal on input line 24 from terminal D. This control signal typically may be of
05 the type from CMOS logic circuitry. The control circuit 20 monitors the voltage across switches 14 and 16 through lines 26 and 28 which are connected to nodes A and B respectively. Also the control circuit 20 monitors the current through switch 14 by lines 30 and
10 32 and monitors the current through switch 16 by lines 34 and 32.

The control means 20 turns on switches 14 and 16 thereby connecting the load to the alternating source 10 in response to the control signal received at
15 terminal D and to a substantially zero voltage crossing of the alternating electrical power of the source 10. The control means 20 turns off switches 14 and 16 in response to the control signal received on terminal D and to a substantially zero current crossing of the
20 alternating electrical power source 10.

This operation of the circuit is shown diagrammatically in Figure 2. Data signal 36 may be a typical logic signal operating between two low voltage levels. For one voltage level the signal indicates an
25 off state for the solid state relay and for a second voltage level the signal indicates an on state for the solid state relay. Curve 38 illustrates the varying voltage of the power source 10. At time point 40 the solid state relay receives a data signal 36 indicating
30 that the solid state relay is to turn on. However, the solid state relay does not turn on until time point 41 where the voltage 38 of the power source 10 crosses the zero axis. At time point 41 the solid state relay turns on connecting the load 12 to the source 10.

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Curves 42 and 44 show the voltage across the load 12 and the current through the load 12, respectively. To illustrate the operation of the present invention the load 12 has been chosen to have a current which is out of phase with the voltage. At time point 46 the data signal 36 instructs the solid state relay to turn off. However, the solid state relay does not turn off until time point 48 when the current through the load 44 crosses the zero point.

Figure 3 is a more detailed block diagram of the present invention including circuit elements within each of the blocks. In the preferred embodiment the first switch 14 and the second switch 16 are field effect transistors (FET) connected in a source to source configuration. The sources of FETs 14 and 16 are connected to node C, the drain of FET 14 is connected to node A and the drain of FET 16 is connected to node B. The gate of FET 14 is connected to the gate of FET 16.

First and second current sensing circuits 50 and 52 are provided. In current sensing circuit 50 FET 54 has its drain connected to the drain of FET 14 and its gate connected to the gate of FET 14. The source of FET 54 is connected to the source of FET 14 through series resistor RS1. When the solid state switch is closed, FET 14 is conducting and the voltage drop across FET 14 is approximately one-half volt for an alternating power source of 110 volts due to the internal resistance of FET 14. Therefore, the voltage drop across RS1 is also approximately one-half volt. Amplifier Q1 measures the voltage across RS1 thereby measuring the current flowing through FET 14. An output signal from amplifier Q1 appears at the output 56 of the current sensing circuit 50 during the

positive half cycle of the AC signal from the source 10 when the solid state relay is on. Operation of the second current sensing circuit 52 is similar to the operation described for the first current sensing circuit 50 and the output signal from Q2 which measures the voltage across RS2 and, therefore the current through FET 16, provides an output signal on the output 58 of the second current sensing circuit 52 during the negative half cycle of the AC signal from the source 10. FETs 54 and 60 provide high voltage protection for amplifiers Q1 and Q2.

Voltage sensing circuit 62 is provided and has first and second resistors R1 and R2 connected between node A and node X, and between node B and node X, respectively. The floating power supply 18 provides a reference voltage to node X through R3. Node X is also connected to the gate of FET 64 which has its source connected to the floating power supply 18 and has its drain connected to an output terminal 66.

Logic circuit 68 is provided and in the preferred embodiment has an OR gate 70 which has its inputs connected to terminals 56 and 58 of the first and second current sensing circuits 50 and 52, respectively. The output of the OR gate 70 is connected to one input of an AND gate 72 and the output of AND gate 72 is connected one input of an OR gate 76. The other input of OR gate 76 is connected to an optical isolator 77 which receives the control signal from terminal D. The output of OR gate 76 is connected to one input of AND gate 78. The other input of AND gate 78 is connected to the output of OR gate 80. One input of OR gate 80 is connected to terminal 66 of the voltage sensing circuit 62 for receiving a voltage sensing signal and the other input of OR gate 80 is

connected to the output AND gate 78. Similarly, the other input of AND gate 72 is connected to the output of AND gate 78. The output of AND gate 78 is also connected to the gates of FET 54 and 60 and in the first and second current sensing circuits 50 and 52, as well as, to the gates of the first and second FET switches 14 and 16. The overall operation of the circuit will now be described.

When the solid state relay is off, FETs 14, 16, 54 and 60 are all also in the off state. The AC signal from the source 10 across FETs 14 and 16 is blocked because of internal diodes D1 and D2. When the relay is on all four FET devices 14, 16, 54 and 60 are on and FETs 14 and 16 therefore create a short circuit connecting the load 22 to the source 10 across nodes A and N.

The relay turns on only at substantially zero voltage crossing of the source 10 and the relay turns off only at substantially zero current crossings of the source 10. When the relay is in the on state amplifier Q1 outputs a signal during the positive half cycle of the AC signal of the source 10 and amplifier Q2 outputs a signal during the negative half cycle of the source 10.

Amplifier Q1 turns off only when the voltage drop across RS1 approaches zero, that is when the current flow through FET 14 approaches zero. Similarly, amplifier Q2 turns off only at the same time as amplifier Q1, that is when the voltage across RS2 approaches zero which is when the current through FET 16 approaches zero. FET 54 and 60 can be turned on only when the output of AND gate 78 is high. When the outputs of amplifiers Q1 and Q2 drop to a low the input to AND gate 72 through OR gate 70 becomes low thereby

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providing an output from AND gate 72 which is low if the input to OR gate 76 from the optical coupler 77 is low, in addition to the signal from the output from AND gate 72 being low. In this case the output of OR
05 gate 76 will be low. If the input to AND gate 78 is low from OR gate 76 then the output of AND gate 78 will be low, thereby causing FET 54, 60, 14 and 16 to turn off. The input to OR gate 76 from the optical coupler 77 is low only when the data input on terminal D to the
10 control circuit 20 is low, thereby indicating that the relay should turn off.

When the relay is off it can be turned on only at the zero voltage crossing. The voltage appearing at node X in the voltage sensing circuit 62
15 is a full wave rectification of the AC signal from the source 10. This is formed by the voltage divider network R1 and R2 connected across nodes A and B. Thus, the voltage at node X is a sign wave of whose amplitude is about one-fifth the value of the AC signal
20 in phase with the AC signal. The voltage across the gate and source of FET 64 is a whole wave rectified sign wave which is positive going. See Figures 4a and 4b. The voltage across the gate and source of FET 64 (V_{xc} in Figure 4b) is viewed by comparing the voltage
25 at node C to Node X (v_c in Figure 4a) and the voltage at node X to node N (v_x in Figure 4a). FET 64 is turned on except for the brief period (in the preferred embodiment approximately 200 microseconds) when the voltage from the gate to source of FET 64 drops to
30 substantially the zero crossing point (V_{zc} in Figure 4b). At this time the input to OR gate 80 connected to the terminal 66 goes high. At all other times the input to OR gate 80 from terminal 66 remains low. When the relay is initially off the output of AND gate 78 is

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at a low and therefore the only time that the output of OR gate 80 can go high is when the input to OR gate 80 from FET 64 goes high. This time is when FET 64 turns off at the substantially zero voltage crossing point of the source 10. When FET 64 is turned off one input to AND gate 78 is high. And gate 78 must receive not only the signal from or gate 80 as a high at the zero voltage crossing point but also must receive a signal through OR gate 76 from the optical coupler 77. The signal from the optical coupler 77 is received only when the control signal from terminal D is received indicating for the relay to turn on. When both inputs to AND gate 78 are high the relay turns on. Once the switch is turned on the output of AND gate 78 is coupled back to the inputs of OR gate 80 and AND gate 72 to hold the relay on until the data input on terminal D goes low and the outputs of amplifiers Q1 and Q2 go low at the substantially zero current crossing point.

The invention is not limited to the particular details of the apparatus and method depicted and other modifications and applications are contemplated. Certain other changes may be made in the above described apparatus and method without departing from the true spirit and scope of the invention herein involved. It is intended, therefore, that the subject matter in the above depiction shall be interpreted as illustrative and not in a limiting sense.

WHAT IS CLAIMED IS:

1. A solid state relay responsive to a control signal and for use with an impedance load and a source of alternating electrical power, said solid state relay comprising:

05 means for turning on said solid state relay operatively connected to the load and the source and responsive to said control signal and to a substantially zero voltage crossing of said alternating electrical power of said source, thereby connecting
10 said load to said source; and

means for turning off said solid state relay operatively connected to the load and the source and responsive to said control signal and to a substantially zero current crossing of said alternating
15 electrical power of said source, thereby disconnecting said load from said source.

2. The device described in Claim 1 wherein said means for turning on said solid state relay comprises:

first switch means operatively connected in series with second switch means for connecting and
05 disconnecting the load to the source, said first and second switch means in series with the load, said source operatively connected across said series connection of said first and second switch means and the load;

10 means for sensing voltage of the source and operatively connected across said first and second switch means and to a common node of said first and second switch means, said voltage sensing means outputting a voltage sensing signal when the source
15 voltage substantially crosses zero;

means for controlling said first and second switch means, said controlling means receiving the control signal and said voltage sensing signal, said controlling means operatively connected to at least
0 said first and second switch means for causing said first and second switch means to turn on or turn off; and

wherein said controlling means turns on said first and second switch means when said controlling
5 means receives said voltage sensing signal indicating substantially zero voltage across said first and second switch means and when the control signal indicates turn on, said turning on of said first and second switch means causing the load to be connected to the source.

3. The device described in Claim 1 wherein said means for turning off said solid state relay comprises:

first switch means operatively connected in
15 series with second switch means for connecting and disconnecting the load to the source, said first and second switch means in series with the load, said source operatively connected across said series connection of said first and second switch means and
20 the load;

first means for sensing current through said first switch means and operatively connected to said first switch means, said first current sensing means outputting a first current sensing signal indicative of
25 substantially zero current flow through said first switch means;

second means for sensing current through said second switch means and operatively connected to said second switch means, said second sensing current means

20 outputting a second current sensing signal indicative
of substantially zero current flow through said second
switch means;

means for controlling said first and second
switch means, said controlling means receiving the
25 control signal and said first and second current
sensing signals, said controlling means operatively
connected to at least said first and second switch
means for causing said first and second switch means to
turn on or turn off; and

30 wherein said controlling means turns off said
first and second switch means when said controlling
means receives said first and second current sensing
signals indicating substantially zero current flow in
said first and second switch means and when the control
35 signal indicates turn off, said turning off of said
first and second switch means causing the load to be
disconnected from the source.

4. A solid state relay responsive to a control
signal and for use with an impedance load and a source
of alternating electrical power, said solid state relay
comprising:

05 first switch means operatively connected in
series with second switch means for connecting and
disconnecting the load to the source, said first and
second switch means in series with the load, said
source operatively connected across said series
10 connection of said first and second switch means and
the load;

first means for sensing current through said
first switch means and operatively connected to said
first switch means, said first current sensing means
15 outputting a first current sensing signal indicative of

substantially zero current flow through said first switch means;

20 second means for sensing current through said second switch means and operatively connected to said second switch means, said second sensing current means outputting a second current sensing signal indicative of substantially zero current flow through said second switch means;

25 means for sensing voltage of the source and operatively connected across said first and second switch means and to a common node of said first and second switch means, said voltage sensing means outputting a voltage sensing signal when the source voltage substantially crosses zero;

30 means for controlling said first and second switch means, said controlling means receiving the control signal, said first and second current sensing signals and said voltage sensing signal, said controlling means operatively connected to at least
35 said first and second switch means for causing said first and second switch means to turn on or turn off; and

wherein said controlling means turns off said first and second switch means when said controlling
40 means receives said first and second current sensing signals indicating substantially zero current flow in said first and second switch means and when the control signal indicates turn off, and wherein said controlling means turns on said first and second switch means when
45 said controlling means receives said voltage sensing signal indicating substantially zero voltage across said first and second switch means and when the control signal indicates turn on, said turning off and on of said first and second switch means causing the load to

50 be disconnected and connected, respectively, to the source.

5. The device described in Claim 4 wherein said first and second switch means are first and second field effect transistors connected in a source to source configuration, said first field effect transistor having its drain connected to the hot side of the source and said second field effect transistor having its drain connected to the load, the load connected between said drain of said second field effect transistor and the neutral side of the source.

6. The device described in Claim 5 wherein said first and second current sensing means are third and fourth field effect transistors, said third field effect transistor having its drain and gate connected respectively, to the drain and gate of the first field effect transistor and having its source connected through a first resistance to the source of the first field effect transistor, said fourth field effect transistor having its drain and gate connected, respectively, to the drain and gate of the second field effect transistor and having its source connected through a second resistance to the source of the second field effect transistor.

7. The device described in Claim 6 wherein said first and second means for sensing current further comprises first and second differential amplifiers having their inputs connected, respectively, across said first and second resistances, an output of said first differential amplifier being the first current sensing signal and the output of the second

differential amplifier being the second current sensing signal.

05 8. The device described in Claim 4 wherein said
voltage sensing means comprises a resistive divider
network connected across said first and second switch
means, a common node of said resistive divider network
operatively connected to a common node of said first
and second switch means such that said common node of
said resistive divider network thereby producing a
series of positive sign wave pulses, said common node
of said resistive divider network operatively connected
10 to an output device for outputting said voltage sensing
signal when the voltage level of said positive sign
wave pulses occurs at substantially a zero level.

05 9. The device described in Claim 8 wherein said
output device is a field effect transistor having its
gate operatively connected to said common node of said
resistive divider network and its source operatively
connected to the common node of said first and second
switch means and its drain having the voltage sensing
signal appearing thereon.

05 10. The device described in Claim 4 wherein said
controlling means comprises a first OR gate for
receiving said first and second current sensing
signals on first and second inputs, an output of said
first OR gate operatively connected to a first input of
a first AND gate, an output of said first AND gate
operatively connected to a first input of a second OR
gate and a second input of said second OR gate
receiving the control signal, an output of said second
10 OR gate operatively connected to a first input of a

second AND gate and a second input of said second AND gate operatively connected to an output of a third OR gate, a first input of said third OR gate operatively receiving said voltage sensing signal, and an output of
15 said second AND gate operatively connected to a second input of said first AND gate and a second input of said third OR gate, said output of said second AND gate operatively connected to at least said first and second switch means.

11. The device described in Claim 10 wherein said first and second switch means are first and second field effect transistors connected in a source to source configuration, said first field effect
05 transistor having its drain connected to the hot side of the source and said second field effect transistor having its drain connected to the load, the load connected between said drain of said second field effect transistor and the neutral side of the source,
10 and wherein said first and second current sensing means are third and fourth field effect transistors, said third field effect transistor having its drain and gate connected, respectively, to the drain and gate of the first field effect transistor and having its source
15 connected through a first resistance to the source of the first field effect transistor, said fourth field effect transistor having its drain and gate connected, respectively, to the drain and gate of the second field effect transistor and having its source connected
20 through a second resistance to the source of the second field effect transistor, and wherein said output of said second AND gate of said controlling means is operatively connected to the gate of said first, second, third and fourth field effect transistors.

12. The device described in Claim 4 wherein said solid state relay further comprises a floating power source means for providing a floating voltage operatively connected to a common node of said first and second switch means and also operatively connected to said voltage sensing means.

13. The device described in Claim 12 wherein said floating voltage source means comprises a first resistor operatively connected to the neutral side of the source in series with a first diode in series with a parallel circuit comprising a capacitor and a zeiner diode which is operatively connected to said common node of said first and second switch means.

14. A method of controlling a solid state relay responsive to a control signal and for use with an impedance load and a source of alternating electrical power, said method comprising:

turning on said solid state relay, said relay operatively connected to the load and the source, in response to said control signal and when there is a substantially zero voltage crossing of said alternating electrical power of said source, thereby connecting said load to said source; and

turning off said solid state relay, said relay operatively connected to the load and the source, in response to said control signal and when there is a substantially zero current crossing of said alternating electrical power of said source, thereby disconnecting said load from said source.

15. Any and all features of novelty described,
referred to, exemplified, or shown.

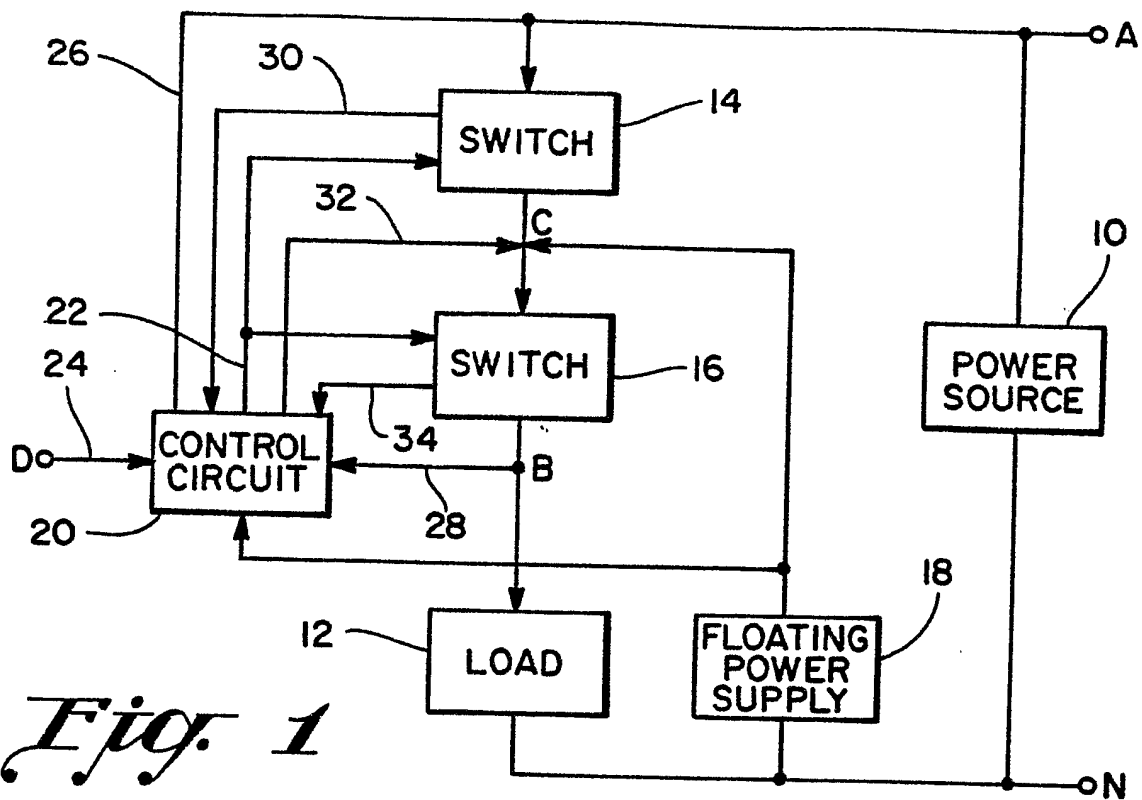


Fig. 1

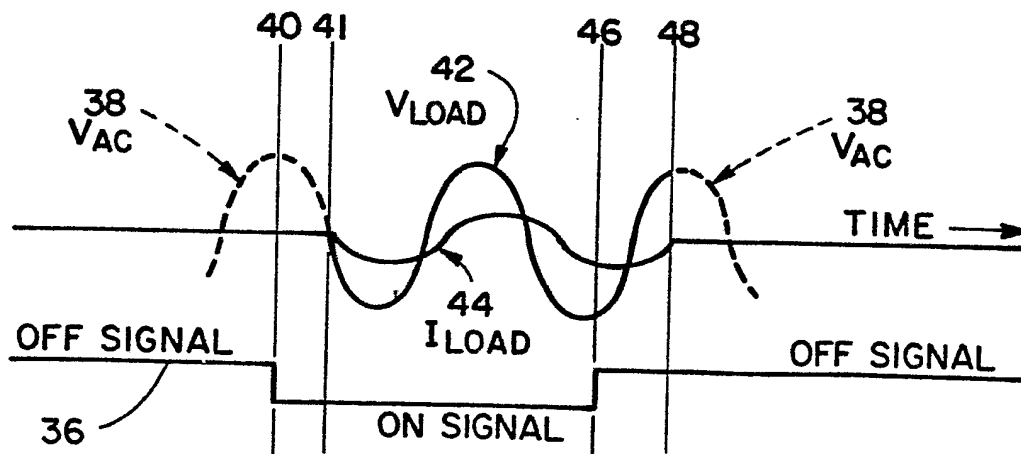
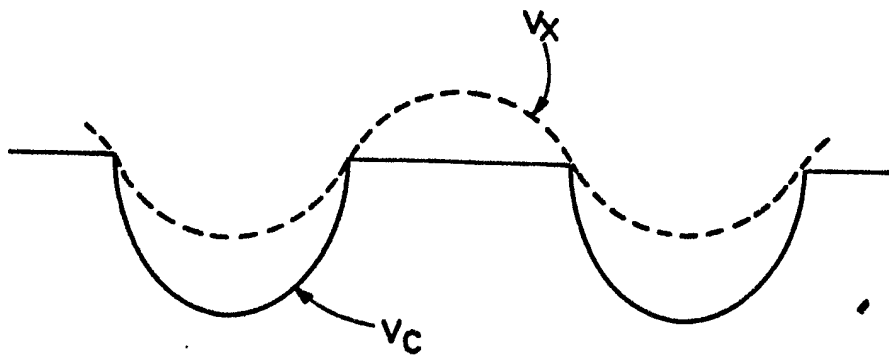
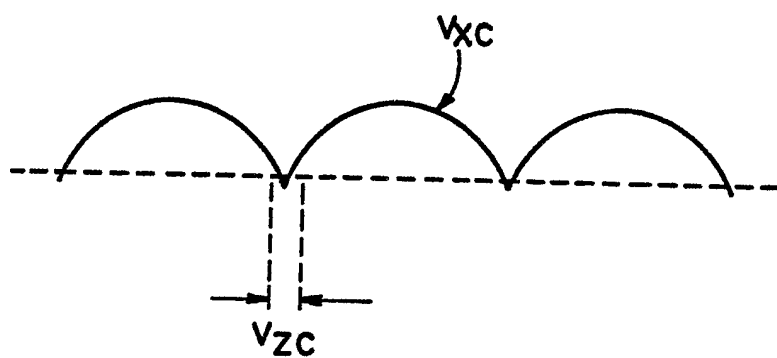


Fig. 2

*Fig. 4A**Fig. 4B*